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1 Three-dimensional drift kinetic response of high beta plasmas in the DIII-D tokamak

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A quantitative interpretation of the experimentally measured high pressure plasma response to externally applied three-dimensional (3D) magnetic field perturbations, across the no-wall Troyon β limit, is achieved. The self-consistent inclusion of the drift kinetic effects in magneto-hydrodynamic (MHD) modeling[1] successfully resolves an outstanding issue of ideal MHD model, which significantly over-predicts the plasma induced field amplification near the no-wall limit, as compared to experiments. The model leads to quantitative agreement not only for the measured field amplitude and toroidal phase, but also for the measured internal 3D displacement of the plasma. The results can be important to the prediction of the reliable plasma behavior in advanced fusion devices, such as ITER [2].

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8 Externally applied, non-axisymmetric magnetic per-
 9 turbations can strongly modify tokamak plasmas, leading
 10 to a three-dimensional (3D) equilibrium. The 3D field
 11 consists of the applied field and the perturbation due to
 12 the perturbed plasma currents [3–5], termed the plasma
 13 response. The plasma response has been systematically
 14 observed for about a decade in tokamak devices e.g. DIII-
 15 D[6–10], JET[11], NSTX [12, 13] and other fusion ex-
 16 perimental devices such as reversed field pinch [14], and
 17 large helical device[15]. In tokamaks, the plasma re-
 18 sponse may significantly amplify the applied field, result-
 19 ing in the neoclassical toroidal viscosity (NTV) [16–18]
 20 and degradation of plasma performance such as the en-
 21 ergetic particle losses[19] and MHD instabilities [20, 21]
 22 in present tokamaks and ITER [2]. Since the initial an-
 23 alytic work by Boozer [5], various attempts have been
 24 made for quantitative modelling of this phenomenon at
 25 high pressure[6, 22], with limited success.

26 In this letter, the drift kinetic effects, derived from
 27 the perturbed drift kinetic theory and associated with
 28 distorted particle orbits by 3D fields [23–25], have, for
 29 the first time, explained the observed beta dependence
 30 of plasma response in the vicinity of the ideal MHD
 31 predicted no-wall β limit, denoted as β^{NW} [26], where
 32 $\beta = 2\mu_0\langle p\rangle/B_0^2$, $\langle p\rangle$ is the volume-averaged plasma pres-
 33 sure, B_0 is the magnetic strength at plasma center, and
 34 μ_0 is the magnetic permeability. A long standing issue in
 35 plasma response physics is that ideal MHD theory finds a
 36 nearly singular amplification of response near β^{NW} due
 37 to the ideal potential energy approaching zero when β
 38 approaches β^{NW} . In contrast, empirical experiments show
 39 the linear increase of plasma response across β^{NW} . This
 40 disagreement is studied through a quantitative compar-
 41 ison between DIII-D experimental results [10] and the
 42 accurate modeling results obtained by solving the lin-
 43 ear hybrid drift-kinetic MHD equation[1]. Since the ki-
 44 netic effects can dramatically modify the plasma response

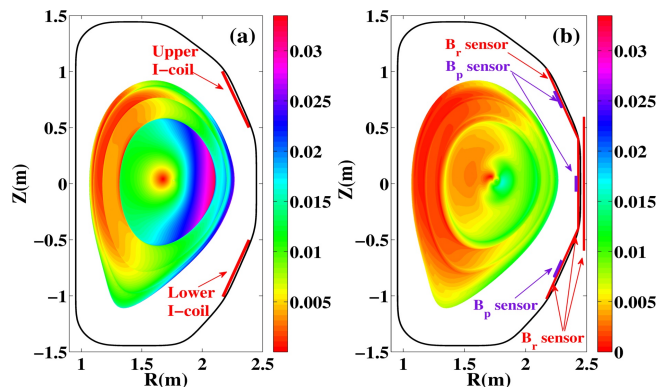


FIG. 1. Comparison of the computed amplitude (cm/kA) of the radial plasma displacement from DIII-D discharge 135773, assuming (a) the fluid model, and (b) the kinetic model. The geometry of magnetic sensors, upper and lower I-coils, and the modelled resistive wall are also shown.

45 structure, the results also highlight the importance of
 46 solving the model equations self-consistently. Only in a
 47 self-consistent calculation, the kinetic effects can modify
 48 the response structure (i.e. displacement).

49 To study the plasma response in DIII-D experiments,
 50 an external $n=1$ traveling perturbation with 10Hz ro-
 51 tating frequency is applied by the upper and lower In-
 52 ternal coil (I-coil) arrays with a toroidal phase differ-
 53 ence $\Delta\phi = 240$ degrees [10]. Neutral beam injection
 54 (NBI) in the plasma current direction is used to con-
 55 trol normalized beta, $\beta_N = \beta(\%)/[I_p(\text{MA})/a(\text{m})B_0(\text{T})]$,
 56 where I_p is the plasma current and a is the plasma
 57 minor radius. β_N^{NW} is the normalized β^{NW} . To in-
 58 vestigate the β dependence of plasma response, the
 59 β_N value of the concerned discharges (135762, 135761,
 60 135758, 135765, 135773, 135759) at 1800ms is varied
 61 from 1.14 to 2.40. The experimental details are pre-
 62 sented in [10, 27]. The magnetic perturbation due

63 to plasma response is defined as $\delta\vec{B}^{plas}$ (Gauss/kA) =
 64 $(\delta\vec{B}^{tot}(\text{Gauss}) - \delta\vec{B}^{ext}(\text{Gauss}))/I_c(\text{kA})$, and is measured
 65 by the magnetic sensor on the low field side. Here,
 66 $\delta\vec{B}^{tot}$ is the total perturbed field. $\delta\vec{B}^{ext}$ is the non-
 67 axisymmetric magnetic perturbation applied by I-coils
 68 with the coil current I_c . Figure 1 illustrate the geometry
 69 of I-coils and magnetic sensors.

70 Since $\delta\vec{B}^{tot}$ is small compared to the equilibrium mag-
 71 netic field \vec{B} in the experiments, $\delta B^{tot}/B < 10^{-3}$, the
 72 comparative results against experiments in this work
 73 demonstrate that the linear perturbation theory is largely
 74 valid for studying 3D plasma response. The linear re-
 75 sponse eventually results from the linear combination
 76 of plasma eigenmode solutions. For instance, the re-
 77 sponse typically results from a single, damped, long-
 78 wavelength kink mode driven by the perturbation. Two
 79 versions of the MARS code are employed in this work.
 80 The MARS-K code solves the linearized ideal single-
 81 fluid MHD equations with drift kinetic effects in the so
 82 called non-perturbative approach [1, 28], where the vac-
 83 uum, the external coils and the modelled resistive wall
 84 (vacuum vessel) as shown in Fig. 1 are included into
 85 the computations [4]. MARS-K is capable of modeling
 86 the plasma response experiment by computing the re-
 87 sponse with self-consistent inclusion of the kinetic effects,
 88 yielding the so-called kinetic plasma response. MARS-F
 89 only solves the linearized ideal MHD equations to obtain
 90 the fluid plasma response [10]. The upgraded MARS-
 91 K/F codes, with improved numerical stability, have been
 92 benchmarked with IPEC-PENT code [29, 30] and MISK
 93 code [31].

94 Figure 1 compares the computed radial plasma dis-
 95 placement $\vec{\xi} \cdot \nabla s$ between the fluid and the kinetic ap-
 96 proaches, based on DIII-D discharge 135773, where the
 97 plasma pressure is close to the $\beta_N^{NW} = 2.25$. Here
 98 $s \equiv \sqrt{\psi}$ with ψ being the normalized equilibrium poloidal
 99 flux [32, 33]. In computing the kinetic plasma response,
 100 the equilibrium distribution function of thermal parti-
 101 cles (TPs, both ions and electrons) is assumed to be
 102 Maxwellian. The energetic particles (EPs), due to NBI,
 103 are modeled with an isotropic slowing down distribution,
 104 with the fast ion pressure and density computed by the
 105 TRANSP code. Both TPs and EPs contribute adiabatic
 106 and non-adiabatic perturbed pressures [1]. In particular,
 107 the non-adiabatic contributions come from the resonant
 108 kinetic effects associated with the particle's toroidal pre-
 109 cession, bounce (for trapped particles) and transit (for
 110 passing particles) motions [1]. The TPs are assumed
 111 to be collisional with the Crook operator as defined in
 112 [25], whereas the EPs are collisionless. In Fig. 1(b),
 113 the plasma response includes all the aforementioned ki-
 114 netic contributions. Compared with the fluid response
 115 shown in Fig. 1(a), the response amplitude is strongly
 116 suppressed by the kinetic effects which significantly mod-
 117 ify the internal structure of the response near the plasma

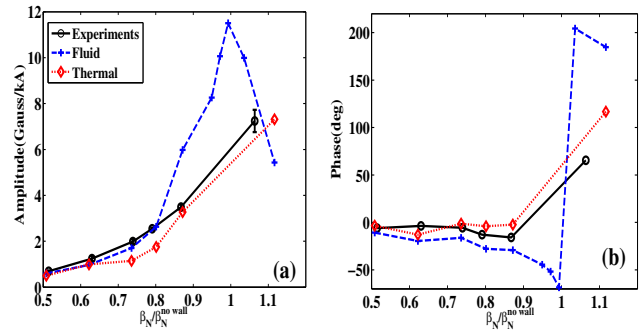


FIG. 2. The β dependence of (a) amplitude and (b) toroidal phase of the response field (δB_r^{plas}) through the magnetic sensors. The computed response, with the fluid model (dashed), and with the kinetic model including thermal particles (diamond), is compared with the experimental data ('o').

118 core at the low field side (LFS).

119 The measured amplitude and toroidal phase of δB_r^{plas} ,
 120 by the radial magnetic sensors located at the LFS mid-
 121 plane, are compared in Fig.2 with that computed by
 122 MARS-F/K. As a subtle point, the wall time of the DIII-
 123 D vacuum vessel has been calibrated in MARS-F/K, by
 124 comparing the computed wall response to the applied ac
 125 fields with frequency scan, with that measured in the
 126 vacuum experiments. In Fig.2, the fluid response agrees
 127 well with experiments for $\beta_N/\beta_N^{NW} < 0.81$, suggesting
 128 that the fluid approximation is adequate for modeling the
 129 plasma response at low beta [10]. This is also supported
 130 by the modeling results for MAST plasmas [34]. How-
 131 ever, the disagreement between the ideal MHD predic-
 132 tion and experiments appears as the pressure approaches
 133 or exceeds β_N^{NW} . Especially, at $\beta_N > \beta_N^{NW}$, ideal MHD
 134 predicts an unstable $n = 1$ resistive wall mode (RWM),
 135 while the experiments remain stable. For computing the
 136 fluid response near β_N^{NW} (β_N/β_N^{NW} from 0.94 to 1.04),
 137 we scale the pressure based on the equilibria from dis-
 138 charges 135773 and 135759 with $\beta_N/\beta_N^{NW} = 0.87$ and
 139 1.06 respectively. The nearly singular amplification of the
 140 fluid response close to the no-wall limit is due to the fact
 141 that the perturbed potential energy $\delta W = \delta W_p + \delta W_{vac}$
 142 approaches zero at β_N^{NW} [12], where δW_p is the plasma
 143 potential energy, δW_{vac} is the vacuum energy, the stable
 144 plasma has $\delta W > 0$. When $\beta_N > \beta_N^{NW}$, the steady state
 145 fluid response losses physics meaning due to RWM in-
 146 stability, although MARS-F can still compute such a re-
 147 sponse (by direct inversion of the system matrix). The
 148 amplitude of the fluid response quickly decreases since
 149 δW becomes finite again. Equally interesting observa-
 150 tion is a significant toroidal phase change (greater than
 151 180 degrees) of the response since δW switches sign. In
 152 contrast, the experimental plasma remains stable. The
 153 measured amplitude of the plasma response almost lin-
 154 early increases with β_N across β_N^{NW} , with 65 degrees less
 155 toroidal phase than the fluid response. The disagree-

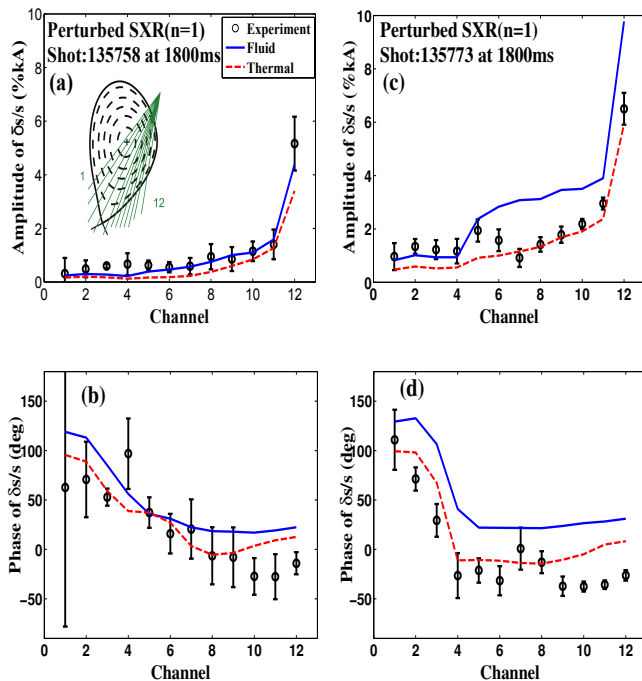


FIG. 3. Comparison of SXR amplitude (a),(c) and phase (b),(d) between the measured ('o') and computed $n=1$ response, where the computed 'fluid' (solid) and 'thermal' (dashed) cases are considered. Two cases are shown: (a),(b) with $\beta_N/\beta_N^{NW} = 0.74$ (135758) and (c),(d) with $\beta_N/\beta_N^{NW} = 0.87$ (135773). The inset in (a) shows the SXR sightline geometry of each channel.

156 ment between the ideal MHD prediction and experiments
 157 points to the need for additional physics, such as the ki-
 158 netic effects [5, 12, 27], in determining the plasma re-
 159 sponse.

160 Much better agreement is obtained by the kinetic re-
 161 sponse computations. The first example (termed 'ther-
 162 mal') is reported in Fig. 2, where the adiabatic contribu-
 163 tions from both TPs and EPs are included, but the non-
 164 adiabatic term includes the TPs contribution only. The
 165 dominant role of TPs on the kinetic response is examined
 166 later on. The kinetic response computations were only
 167 performed for equilibria reconstructed from experiments,
 168 i.e. no pressure scaling near β_N^{NW} as has been made
 169 for the fluid response computations. This is because the
 170 drift kinetic computations require additional experimen-
 171 tal profiles that cannot be simply scaled, such as the
 172 $E \times B$ rotation, the pressure profile of EPs, etc. The
 173 kinetic response significantly improves agreement with
 174 experiments near or above β_N^{NW} due to several factors.
 175 (i) The kinetic effects modify the plasma response struc-
 176 ture as shown in Fig. 1, which also changes δW . (ii)
 177 The kinetic effects result in a complex dissipative kinetic
 178 energy δW_K [35] which acts to maintain a finite response
 179 amplitude as the pressure approaches or exceeds the no-
 180 wall limit. (iii) The finite imaginary part of δW_K also

181 reduces the toroidal phase shift compared to that of the
 182 fluid response, leading to a much closer agreement (of
 183 the kinetic response) to experiments. (iv) Finally, the
 184 hybrid kinetic-MHD theory predicts stable RWM in the
 185 highest β case (135759), which is consistent with the ex-
 186 perimental observation. Similarly, the kinetic response
 187 also shows the reliable agreement with NSTX plasma re-
 188 sponse experiments which cannot be predicted by the
 189 fluid response [36].

190 We also note that the present kinetic computations
 191 tend to slightly underestimate the experimental response
 192 amplitude at low beta $0.7 < \beta_N/\beta_N^{NW} < 0.9$. This may
 193 point to certain missing physics in our present kinetic
 194 model. One likely candidate is the perturbed electro-
 195 static potential which is neglected in MARS-K. The un-
 196 certainties in the reconstructed plasma edge rotation may
 197 also contribute to this discrepancy.

198 Another crucial validation of the kinetic response
 199 model is the direct comparison of the computed and mea-
 200 sured internal response structure. In experiments, the
 201 internal structure is derived from the soft x-ray (SXR)
 202 measurement [37]. This is compared with computations
 203 in Fig. 3 for two discharges. The experimental data
 204 are represented by a quantity $\delta s/s$, measured at 12 SXR
 205 channels shown in Fig. 3(a), where the equilibrium ($n=0$)
 206 SXR measurement, $s(m)$, and the $n=1$ component of the
 207 SXR perturbation, $\delta s(m/kA)$, are both integral quanti-
 208 ties along the sightline of each channel. This quantity
 209 is compared to the internal structure of the $n=1$ plasma
 210 response predicted by MARS-F/K via modeling of the
 211 SXR measurements. Details of modeling are described in
 212 [27]. In Fig. 3, the experimental data are time-averaged
 213 over 400ms (4 cycles of SXR) around 1800ms. The error
 214 bars are obtained from an error analysis of the data
 215 fitting. The simulated SXR signals, for the 'fluid' and
 216 'thermal' cases, are based on the computed normal dis-
 217 placement of the plasma response. The phase of $\delta s/s$
 218 is defined with reference to $\delta \vec{B}^{ext}$ of upper I-coils. For
 219 the low β case ($\beta_N/\beta_N^{NW} = 0.74$), both fluid and kinetic
 220 computations show agreement with experiments, for both
 221 amplitude and phase of the $n=1$ internal structure. We
 222 note that the largest perturbed amplitude appears near
 223 the plasma edge (channel 12). For the case near the no-
 224 wall limit ($\beta_N/\beta_N^{NW} = 0.87$), the fluid response largely
 225 overestimates the amplitude of the internal perturbation
 226 along channels 6 to 12. The phase of the fluid response
 227 also disagrees with measurements. The kinetic response
 228 ('thermal' case), on the other hand, generally shows very
 229 good quantitative agreement with DIII-D experiments,
 230 for both amplitude and phase. The above comparison
 231 again indicates that the kinetic effects play an important
 232 role in the high beta plasma response. The self-consistent
 233 hybrid drift-kinetic MHD theory is further validated by
 234 this sophisticated SXR comparison. It is noted that this
 235 modification of plasma response by kinetic effects near
 236 β_N^{NW} can be critical to many important applications such

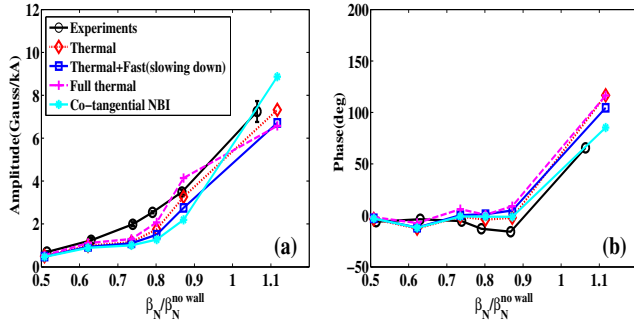


FIG. 4. The β dependence of (a) amplitude and (b) toroidal phase of δB_r^{plas} . The experimentally measured δB_r^{plas} is compared with the computed kinetic response of 'thermal' (diamond), 'thermal+fast' (square), 'full thermal' ('+') and 'co-tangential NBI' ('*') cases

237 as NTV torque, which has the quadratic dependence on
 238 the perturbed field and the displacement. For instance,
 239 figure 3 (c) implies the fluid response might predict four
 240 time larger NTV torque than the more accurate kinetic
 242 response.

243 Further MARS-K computations reveal that the kinetic
 244 effects from thermal particles play the major role in re-
 245 producing the experimental plasma response. Figure 4
 246 compares results under various assumptions on the par-
 247 ticle contributions. By adding the non-adiabatic con-
 248 tributions from EPs on top of "thermal" case, termed
 249 "thermal+fast", we find negligible impact of EPs on the
 250 kinetic response. On the other hand, by assuming that all
 251 the equilibrium pressure comes from TPs (termed "full
 252 thermal" case), the kinetic response shows similar be-
 253 havior as that of the "thermal" case. Near the no-wall
 254 limit, the response amplitude in the "full thermal" case is
 255 slightly larger than that of the other two cases, due to the
 256 lack of one extra adiabatic term arising from the bound-
 257 ary integration in the particle phase space for the slowing
 258 down EPs with finite birth energy [28]. This extra term
 259 eventually plays a damping role. Further comparison
 260 of the SXR based internal structure again confirms the
 261 importance of thermal particle contribution, at least for
 262 these DIII-D plasmas. In experiments, co-tangential NBI
 263 was employed, with two injection tangency radii of 76cm
 264 and 115cm, producing EPs with anisotropic distributions
 265 in the particle pitch angle space. This motivates us to
 266 test the sensitivity of kinetic response against the EP
 267 models. MARS-K has implemented an anisotropic NBI
 268 model which is suitable for ITER [28]. We choose an aver-
 269 aged injection tangency radii of 95.5cm and an ITER-like
 270 beam width parameter ($\delta\zeta = 0.123$). The results, termed
 271 "co-tangential NBI" in Fig. 4, show that the plasma re-
 272 sponse has a larger amplitude than other cases due to
 273 the destabilizing effect of EPs and a better phase agree-
 274 ment with experiments at $\beta_N/\beta_N^{NW} = 1.12$. It implies
 275 experimentally more relevant NBI models should be im-

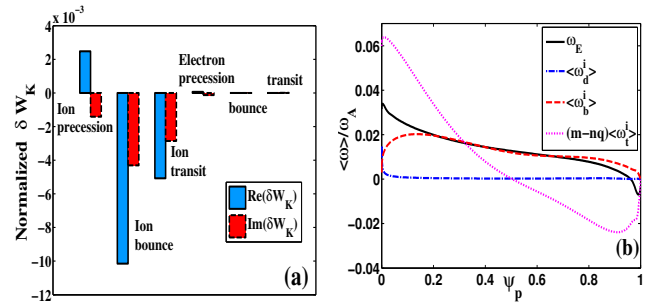


FIG. 5. (a) The real and imaginary parts of normalized δW_K contributed by different resonances of thermal ions and electrons. (b) The radial profiles of ω_E (solid) and various averaged frequencies of trapped and passing thermal ions over the velocity space and the flux surface, such as $\langle\omega_a^i\rangle$ (dash-dot), $\langle\omega_b^i\rangle$ (dashed) and $(m-nq)\langle\omega_c^i\rangle$ (dotted) of thermal ions. All frequencies are normalized by the Alfvén frequency ω_A at the plasma center.

276 plemented in the future to better capture the EPs kinetic
 277 effects at high beta. Nevertheless, for these DIII-D plas-
 278 mas, the TPs contribution is still dominant, and the mod-
 279 eled monotonic increase of the response amplitude with
 280 pressure is qualitatively unchanged by the anisotropic EP
 281 model.

282 A deeper understanding of the kinetic response physics
 283 is gained by the energy analysis shown in Fig. 5(a), where
 284 we compare the non-adiabatic kinetic contributions from
 285 both thermal ions and electrons, in various resonance
 286 regimes including toroidal precession and bounce reso-
 287 nance of trapped particles, as well as transit resonance
 288 of passing particles. We choose discharge 135773 with
 289 $\beta_N/\beta_N^{NW} = 0.87$ to illustrate these physics. Figure 5(a)
 290 presents the real and imaginary parts of δW_K associated
 291 with the aforementioned kinetic contributions. These en-
 292 ergy components are normalized by the plasma volume
 293 integrated inertia $\delta K = \int \rho(\xi \cdot \nabla s)^2 dV$, where ρ is the
 294 mass density. The comparison shows that thermal elec-
 295 trons contribute much less δW_K than thermal ions, since
 296 the former have much higher collision, bounce, and tran-
 297 sit frequencies than the latter. Moreover, we find that
 298 the precession, bounce and transit resonances of thermal
 299 ions contribute comparable amounts of δW_K , indicating
 300 that three types of resonances from TPs are important for
 301 the kinetic response. The eventual response depends on
 302 the net contribution, after possible cancellations among
 303 all energy components. In Fig. 5(b), the frequency com-
 304 parison confirms the energy analysis results. It is clear
 305 that the $E \times B$ rotation can always be in local resonance
 306 with all types of particle drift motions, due to the energy
 307 dependence of particle drift frequencies [38]. Indeed, ω_E
 308 can match, at different flux surfaces, the averaged preces-
 309 sion frequency $\langle\omega_a^i\rangle$, the bounce frequency $\langle\omega_b^i\rangle$, as well
 310 as the transit frequency $(m-nq)\langle\omega_c^i\rangle$ of thermal ions,
 311 where m is the poloidal mode number, q is the safety fac-

tor. The harmonic numbers $l = 1$, $m = 2$ and $n = 1$ are chosen because these belong to the dominant harmonics contributing to the plasma response.

In summary, kinetic response resolves the long-standing disagreement between the fluid theory prediction and the experimental observations, as long as the plasma pressure approaches or exceeds the no-wall limit. Quantitative comparison between the measured $n = 1$ plasma response (both external and internal data), and the computational results, reveals the key importance of kinetic effects from TPs. Kinetic response leads to internal structure that is different from the fluid response throughout the plasma. The energy analysis shows that the modification of the response is mainly contributed by the precession, bounce and transit resonances of thermal ions in these DIII-D plasmas. These results demonstrate the validity of the hybrid drift-kinetic MHD model, and highlight the necessity of self-consistent approach as the only viable way for achieving quantitative modeling of 3D plasma response in high beta tokamak plasmas.

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