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Prepared for the U.S. Department of Energy under Contract DE-AC02-09CH11466.

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Suitability of 3D Printed Plastic Parts for Laboratory Use

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(Dated: February 3, 2014)

Abstract

3D printing has become popular for a variety of users, from industrial to scientific to the home hobbyist. In order to determine the suitability of 3D printed parts for the laboratory, we measured the accuracy, strength, vacuum compatibility, and electrical properties of pieces printed in plastic. The flexibility of rapidly creating custom parts has quickly led to the 3D printer becoming an invaluable resource in our laboratory.

I. INTRODUCTION

Additive printing of material, commonly known as 3D printing, has the potential to revolutionize manufacturing for both industrial and consumer use.[?] These printers come in different sizes and configurations and work with a variety of materials including plastics, metals, ceramics, and organic material. The most inexpensive desktop printers currently print in plastic and cost less than \$3,000, with entry-level devices costing less than \$1,000. One straightforward application of a 3D printer is rapid prototyping of a new design and they have gained significant popularity with the DIY (do it yourself) community.

3D printing of laboratory parts has several potential advantages including significant cost savings, customization of a standard part for a specific function, and rapid access when compared to ordering from a commercial source. Recently, Zhang et al have developed a library of open-source files for printing optics equipment.[?] They found a cost savings of up to 97% compared to the equivalent objects purchased commercially. Their designs are available for free download on the web site Thingiverse, a portal for open source designs of a variety of objects.[?]

Cost is not the only important consideration, it is obviously crucial that printed parts be of suitable quality to not add new sources of error to an experiment beyond what might be expected from the equivalent commercially available equipment. For example, Povilus et al.[?] looked at the vacuum compatibility of a variety of 3D printed materials (glass, acrylic, plastic, and sterling silver) for ultrahigh vacuum environments ($< 10^{-8}$ torr) and found that, unsurprisingly, only sterling silver had a low enough outgassing rate to be suitable for experimental use.

In this work, our primary goal was to determine the suitability of printed objects for a plasma physics laboratory where the required pressures are more moderate. However, our experimental parameters are typical for many applications and these results should be relevant to experimenters in a large variety of fields. Our experimental conditions range from atmospheric pressure to 10^{-6} torr, with voltages on metal electrodes ranging from 0.5 - 15 kV at frequencies that range from DC to 200 kHz.

After a brief description of the printer used for these measurements (Sec. II), we present our results on the accuracy (Sec. IIIA) of a printed part by comparing the dimensions of the part to the dimensions of the drawing used to create it. Strength (Sec. IIIB) of these

plastic parts was determined by measuring the maximum load before breaking. Vacuum compatibility (Sec. IIIC) was determined by looking at the outgassing by the plastic at various temperatures. The electrical (Sec. IIID) properties of printed parts was estimated by printing plastic insulators around high voltage electrodes and observing the plasma discharges produced. Finally, we give some examples of how we are using 3D printed parts in our laboratory.

II. 3D PRINTER

While there are a variety of printers currently available for purchase and versions of the open source RepRap printer[?] can be built for less than \$1,000, we chose to use the Replicator 2 from Makerbot Industries[?] based upon the cost, maximum size of objects that can be printed, resolution, and reliability. The printer offers a maximum build volume of 28.5 cm x 15.3 cm x 15.5 cm and a minimum layer height of 100 μ m. The manufacturer claims a positioning precision of 11 μ m in XY and 2.5 μ m in Z, though we found (see below) that the error in accuracy was significantly larger than the precision. The Replicator 2 prints only in polylactic acid (PLA), a biodegradable plastic commonly made from corn starch or sugar cane. PLA for this printer is sold in 1 kg spools of 1.75 mm diameter filament that is heated by the printer to a temperature of 230°C and extruded through a 0.4 mm diameter nozzle. Individual layers of plastic are extruded in the X-Y plane and then the distance between the extruder and the build platform is increased in the Z-direction and another layer is printed. This continues until the full three dimensional object is completed.

To do this, software provided free by the manufacturer converts a *STL, *OBJ, or *THING file produced by most computer aided design (CAD) software into horizontal slices (the g-code) that provides instructions to the printer of where to extrude plastic in X, Y, and Z. There are several excellent free examples of CAD software such as openSCAD,[?] SketchUp,[?] 123d Design,[?] or Blender[?] that can be used if a commercially available option is not available to the experimenter.

In general, one prints a complete object from start to finish but it is also possible to modify an object during or after a print. For example, one can directly print a hole that includes threads sized to match a screw (and of course one can print a screw), but it is simpler to simply print a properly sized hole and cut the threads with a normal tap used

to create threads in metal. One can also embed other material into the plastic if necessary. (see Sec. IIIC) In one of our experiments, we made a sandwich of PLA insulation around a thin sheet of copper that served as one electrode of our system. To manufacture this, we paused the printer when it was 50% complete, placed the copper onto the exposed top layer of the print, and then resumed the print. That way, we were able to have insulation of equal thickness on both sides of the copper though this method can be used to embed material into a print at any point in the process.

III. RESULTS

A. Accuracy

The software provided with the printer has three default resolutions settings, low, medium, and high which correspond to a layer thickness of $300\ \mu\text{m}$, $200\ \mu\text{m}$, and $100\ \mu\text{m}$ respectively. The user controls the layer thickness, the number of outer layers that are printed (the shells), and the percent of the object that is solid (the infill) from 10 - 100%. (See Figure 1) Two solid shell layers are sufficient to create a rigid body even for an infill of 10%. In general, print speed is proportional to layer thickness, e.g., an object printed with

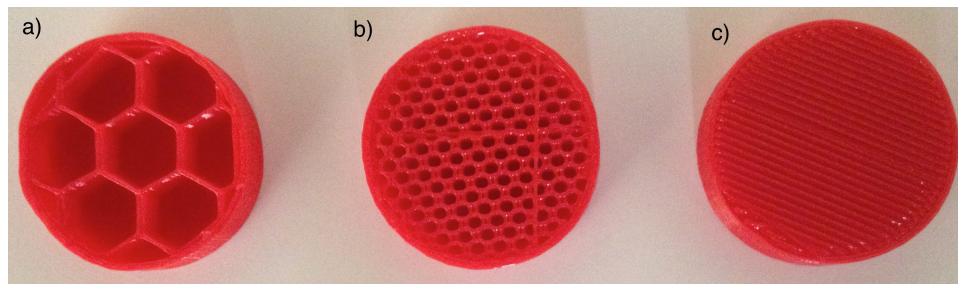


FIG. 1. A cylinder printed with $0.2\ \mu\text{m}$ layer thickness, two solid outer shells, and a) 10% infill, b) 50% infill, and c) 100% infill.

$200\ \mu\text{m}$ layers takes half the time of the same object printed at $100\ \mu\text{m}$ layers. At a $300\ \mu\text{m}$ layer height, print speed is relatively fast and is helpful for quickly testing the printability of a newly designed object, but the thickness of the individual layers gives a surface roughness that we deemed insufficient for our needs and we did not use this setting in any of our tests.

Accuracy in the dimensions of a printed object is a function of the layer thickness. We tested a variety of shapes (pyramid, cone, cube, cylinder) and compared the measured

dimensions with the original CAD drawing dimensions. Each object was printed at least twice and the measurement of the dimensions averaged. In general, the shape of the object did not matter and, as one would expect, the primary parameter of interest was the thickness of each layer. The average error for all objects printed was on the order of 1-2 times the layer height. For example, a 25.4 mm x 6.35 mm cylinder had an average error of around 0.44 mm for a layer height of 200 μm while the same cylinder printed with a layer thickness of 100 μm had an average error of approximately 0.16 mm. Clearly, for high precision objects 3D printing is not suitable, but there are many applications in the laboratory where this level of accuracy is more than sufficient and we give several examples from our laboratory below.

B. Strength

Given that these are plastic parts, an obvious question is how strong they are and what load is required before they will deform or break. To quantify this, we used a Tines Olsen Model 1000 Universal Testing machine to determine the ultimate tensile strength of our test objects. This is the maximum stress that a material can withstand while being pulled before breaking. The printed pieces were bars 0.125 x 0.5 x 6 inches. The bars were pulled lengthwise by the ends up to a maximum load of 1,000 lbs. Individual pieces were inserted into the machine and the load was increased until the sample broke.

Test pieces were printed so that the externally applied load was distributed along all layers. In other words, we wanted to make sure that we were not measuring the force needed to separate individual layers, which is much smaller than the force needed to break an object when applied along the layers. (See Figure 2) For an experimenter concerned about the load on a printed object, this is an important design concern. Fortunately, it is a simple issue to address and, in most cases, one can simply orient the virtual object before printing so that the layer axis is always perpendicular to the expected direction of the experimental load.

Printed test pieces were varied by infill percentage, from 100% (solid) down to 10%. All measurements were taken at a room temperature of 20°C. As the load was increased, there was no deformation of the samples before the fracture occurred. This is called a brittle failure, as is commonly seen in glass or ceramic rather than most polymers. The solid

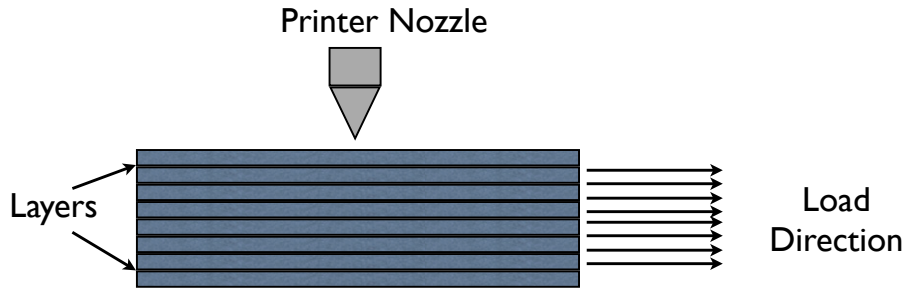


FIG. 2. Schematic of a printed bar showing the layer direction and the load direction. The printer nozzle is drawn for reference.

(100%) samples broke with an average applied force of 8,800 psi, reasonably close to the published value of 7,600 psi for bulk PLA.[?] As the percentage of infill decreased, there was a linear decrease in the tensile strength with a minimum measured strength of 5040 psi for a 10% infill. For comparison, that is what one might expect across the grain from a piece of wood.[?]

C. Vacuum Compatibility

Our interest in 3D printed parts for the laboratory started with the question of whether they would be suitable for the inside of a vacuum vessel at moderately low pressures near high voltage electrodes used to create a plasma. Typically, plastic is assumed to be a poor choice for most vacuum experiments due to the relatively high vapor pressure that introduces impurities into a clean system and causes an unacceptable increase in the base pressure of the vessel. Thus, we started with the question of how a printed plastic part would behave in the moderately low pressures of our experiments (1×10^{-6} torr $< p < 760$ torr) at both room and elevated temperatures.

Our experimental setup consisted of a Residual Gas Analyzer (RGA) attached to a vacuum sealed oven capable of reaching a maximum temperature of 800°C. The oven was pumped by a 150 l/s turbo molecular pump to a base pressure of approximately 1.0×10^{-6} torr. Background scans from the RGA showed measurable levels of hydrogen, nitrogen, and water vapor. The vacuum chamber pressure was then vented with nitrogen gas and printed pieces of different shapes and infill percentages with a maximum weight of up to 20

g were inserted into the vacuum chamber and the background gas was evacuated. At room temperature the RGA showed no measurable increase in the background signals and the overall base pressure did not increase, indicating that any outgassing from the plastic was insignificant at these moderate pressures regardless of the infill percentage. Our assumption is that the printed parts are porous enough that any trapped air volume is rapidly evacuated from the interior of the part and the vapor pressure of the plastic was small.

The temperature of the chamber was then systematically increased while the RGA signals were monitored. Background impurity levels increased as the temperature increased, but it was not until the temperature reached 75°C that any measurable signal due to hydrocarbons from the plastic was observed, indicated by an increase in the RGA signal for AMU values of 39 and greater. Note that this threshold is much lower from the extrusion temperature for PLA plastic of 230°C. Thus, as long as the bulk temperature of a printed part is below approximately 75°C, it is possible to use these moderate vacuums without contaminating the system.

To confirm this result in actual experimental conditions, we inserted a test piece into the vacuum chamber of a DC glow discharge plasma experiment. After evacuating the chamber, argon gas was introduced into the system until the equilibrium pressure was to 0.1 torr. Two stainless steel electrodes were attached to a power supply and the voltage increased until the argon gas became conductive and a plasma was formed at 500 V with a current of 10 mA. The plasma was sustained for 5 hours, during which there was no measurable change in the experimental conditions (base pressure, voltage, or discharge current) and no visible change in the plastic.

D. Use as a Dielectric

A dielectric barrier discharge (DBD) consists of two electrodes separated by a dielectric barrier. DBDs have a variety of applications including ozone generation, surface modifications, water treatment, and plasma medicine. Here, we looked at how the thickness and density of 3D printed electrodes affects the formation of microdischarges from a DBD. The electrodes were thin pieces of copper tape surrounded by PLA plastic. The DBD setup consisted of a cylindrical aluminum HV electrode surrounded by a layer of 6 mm thick alumina and connected to a 15 kV, 75-300 kHz, AC power supply (Figure 3). The printed electrodes

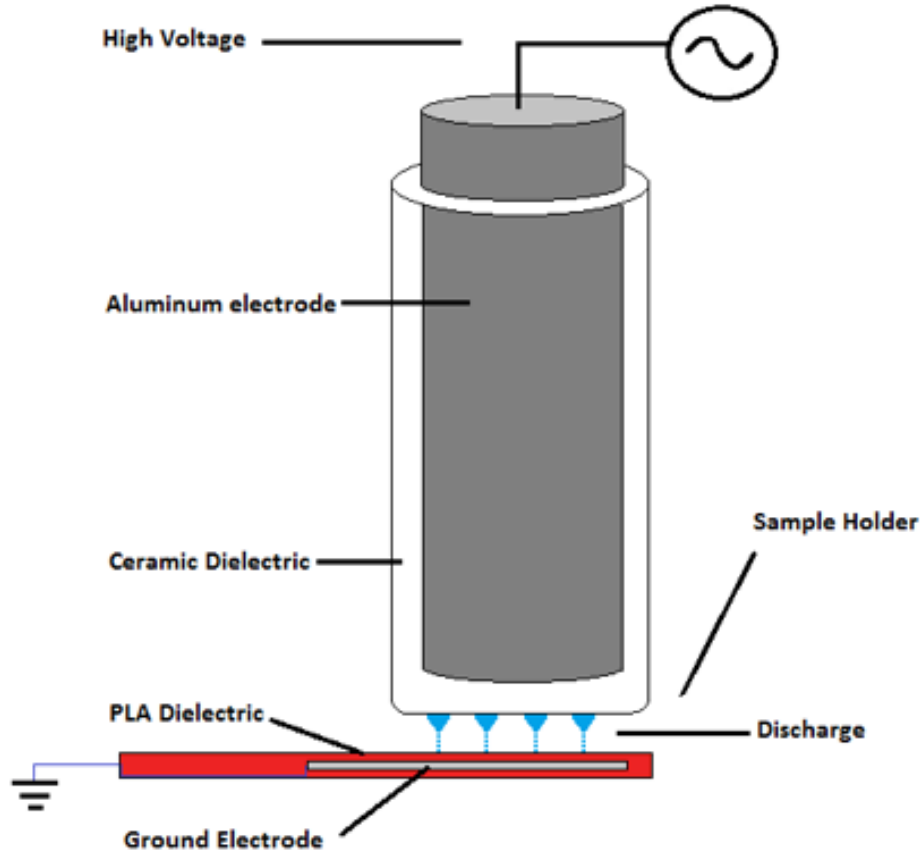


FIG. 3. Schematic diagram of a dielectric barrier discharge (DBD) showing a printed electrode used as ground.

were 12 cm long, 2 cm wide, and 0.4 cm thick. They were grounded and held 5 mm beneath the alumina, forming a discharge gap. The DBD was operated with an Ar/Air gas mixture at atmospheric pressure. An intensified CCD camera was used to image the microdischarges at various stages of their development.

Each image was analyzed by counting the number of visible microdischarges that appeared. The number of observed discharges for each image was averaged over all of the images for each electrode and the infill percentage was varied between 10-100% for electrodes of the same configuration.

Typically, a DBD consists of a large number of low current discharges. Here, printed electrodes with a larger infill percentage had a higher number of microdischarges form than the equivalent electrode with less plastic in the interior. As the number of discharges decreased, the current of the individual discharges also increased though the total current in the system

was roughly constant. These higher current microdischarges often created an electrical arc that damaged the electrode. Thus, the electrodes printed with the greatest infill percentage performed best and the ability to print dielectric material in any size, shape, or configuration provided an unmatched flexibility to quickly and efficiently test new configuration ideas for different experimental conditions.

IV. EXAMPLES

Besides their use as electrodes, we use printed parts to create duplicates of damaged or lost pieces and we design original objects for specific applications. Our most common application is to hold or clamp another piece of equipment. For example, Figure 5a shows printed parts used to hold electrodes in our Planeterrella[?], an aurora borealis demonstration. Figure 5b shows a replacement handle for a piece of test equipment, while Figure 5c shows a cooling fan for electronics (with a laboratory logo added as a whimsical touch). The versatility of the printer is such that our first reaction to an equipment need is no longer whether we can find or purchase the required piece of equipment, but can we print it.

V. CONCLUSION

In order to test the suitability of 3D printed parts for laboratory use, we performed a series of tests on material printed by a widely available commercial printer. Strength, accuracy, vacuum compatibility, and electrical dielectric properties were all found to be sufficient for many common laboratory needs. The printer is now a crucial piece of our laboratory and used regularly. Additionally, a 3D printer is an exceptional tool for motivating students to learn CAD drawing techniques and they are able to readily learn how to design and build a variety of custom made parts.

ACKNOWLEDGMENTS

We gratefully thank Arturo Dominguez, Andy Carpe, Larry Guttadora, Deedee Ortiz, and Shannon Greco for many fruitful discussions and assistance with the results reported here. In addition, Stephen Jurczynski's help with the tensile strength measurements were



FIG. 4. Photographs of printed parts in a) Planeterrella holding up aluminum spheres, b) replacement handle, and c) protective cover.

invaluable.

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¹ New Media Consortium Horizon Report: 2013 Higher Education Edition, <<http://www.nmc.org/pdf/2013-horizon-report-HE.pdf>>.

² Zhang C, Anzalone NC, Faria RP, Pearce JM (2013) Open-Source 3D-Printable Optics Equipment. PLoS ONE 8(3): e59840.

³ <http://reprap.org>.

⁴ <http://www.thingiverse.com>.

⁵ A. P. Povilus, C. J. Wurden, Z. Vendeiro, M. Baquero-Ruiz, J. Fajans, Vacuum Compatibility of 3D-Printed Materials, arXiv:1308.4962, <http://arxiv.org/pdf/1308.4962v2.pdf/>>.

⁶ <http://www.makerbot.com>

⁷ <http://www.openscad.org>

⁸ <http://www.sketchup.com>

⁹ <http://www.123dapp.com/design/>

¹⁰ <http://www.blender.org>

¹¹ <http://plastics.ides.com/generics/34/c/t/polylactic-acid-pla-properties-processing>

¹² http://en.wikipedia.org/wiki/Ultimate_tensile_strength

¹³ <http://planeterrella.obs.ujf-grenoble.fr>

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